

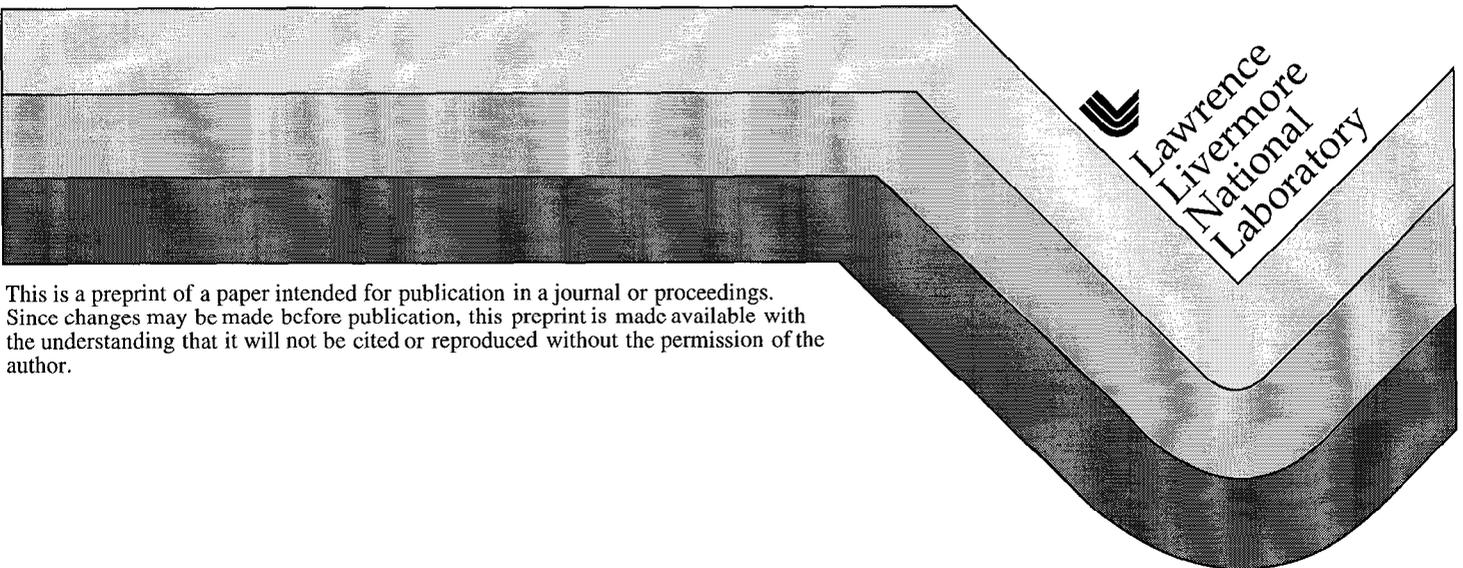
UCRL-JC-135091
PREPRINT

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This paper was prepared for submittal to the
1999 Oil and Gas Conference
Technology Options for Producer Survival
Dallas, TX
June 28-30, 1999

July 20, 1999



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Electrical resistance tomography using steel cased boreholes as long electrodes

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Abstract

Electrical resistance tomography (ERT) using multiple electrodes installed in boreholes has been shown to be useful for both site characterization and process monitoring. In some cases, however, installing multiple downhole electrodes is too costly (e.g., deep targets) or risky (e.g., contaminated sites). For these cases we have examined the possibility of using the steel casings of existing boreholes as electrodes. Several possibilities can be considered. The first case we investigated uses an array of steel casings as electrodes. This results in very few data and thus requires additional constraints to limit the domain of possible inverse solutions. Simulations indicate that the spatial resolution and sensitivity are understandably low but it is possible to coarsely map the lateral extent of subsurface processes such as steam floods. The second case uses an array of traditional point borehole electrodes combined with long-conductor electrodes (steel casings). Although this arrangement provides more data, in many cases it results in poor reconstructions of test targets. Results indicate that this method may hold promise for low resolution imaging where steel casings can be used as electrodes but the merits depend strongly on details of each application. Field tests using these configurations are currently being conducted.

Background

Electrical resistance tomography (ERT) has been demonstrated to be a useful characterization tool, providing details of the lithostratigraphy between wells (e.g., Newmark *et al.*, 1994). ERT has previously been used to map subsurface processes such as fluid infiltration (Daily *et al.*, 1992), steam injection and ohmic heating (Ramirez *et al.*, 1993, 1995) by mapping the spatial and temporal changes in soil resistivity resulting from changes in liquid saturation and temperature. It has also been used to monitor the removal of DNAPL chemical during pumping (Newmark *et al.*, 1998). The presence of appreciable amounts of separate-phase, electrically insulating fluids locally increase electrical resistivity. The removal of these fluids during pumping produces a drop in electrical resistivity, as the insulating fluids are displaced by relatively conductive formation fluid.

In general, ERT has been conducted using a cross-borehole geometry, using multiple electrically-isolated electrodes placed in vertical arrays. This geometry has the potential to

produce relatively high quality, high resolution images when the aspect ratio of vertical to horizontal spacing is equal to or greater than 1.5:1.0. Typical electrode installations involve multiple electrodes strung on nonconductive casing (e.g., plastic or fiberglass) in conventionally-installed boreholes, or as instrumentation strings installed using cone penetrometers. Both designs have been effective in shallow to moderate depths (most recently up to 1300 ft), but deeper installations require significant and more costly modifications. The ability to obtain ERT images using existing conventional casings as electrodes would increase the applicability of the technique. In this context, we undertook a study to examine the possibility of using the steel casings of existing boreholes as electrodes.

The method of ERT data collection and processing has been described in detail by Ramirez and his colleagues (e.g., Ramirez *et al.*, 1995). The forward and inverse modeling codes are described by LaBrecque *et al.*, (1996). The forward solution is implemented using the finite difference technique with Newman boundary conditions at the ground air interface and Dirichlet boundary conditions along the other faces of the cube. The inverse solution employs an objective function which aims to minimize data misfit and model roughness. The minimization of the objective function is done iteratively.

Case 1: Crosswell ERT

In the first case, we modeled ERT data acquired using a standard crosswell configuration. The model simulates a typical layered sand and shale sequence common in many oil fields (Figure 1). It is composed of a series of various thickness, 40 ohm-m units (sands) imbedded in a 4 ohm-m matrix (shales). The sand units range in thickness from 2.3 m to 9.1 m thick. These 2D simulations include two ERT electrode strings separated by 30.5 m, each consisting of 30 electrodes. Vertical electrode spacing is set to 4.6 m, so the 2.3 m thick sand is half the electrode spacing. In all models, there are two pixels per electrode spacing (each pixel in this first case is about 2.3 m square). The modeled region is larger than the image plane alone, so boundary effects are minimized. Synthetic data generated using the forward model is inverted, producing an image indicative of a typical baseline image one might obtain in the field. In the baseline inversion, the shape of the sands are well represented, even the one whose thickness is only half the electrode separation. The amplitudes are also well reconstructed except for the thinnest sand layer, whose amplitude reflects the averaging expected over the electrode spacing.

We next decrease the resistivity in the sand units, as we simulate the passage of steam through the sands. Over time, the sand units fill with steam, decreasing their resistivity to that of the surrounding shale (4 ohm m). As the steam fills the sands, the inverted images clearly indicate the location of the steamed region. Amplitudes are similarly reproduced as for the baseline image. The location and extent of the region in which resistivities are decreased is well reproduced in all but the thinnest sand, where it appears to be somewhat smeared laterally beyond the zone of change in the model. The absolute value of the difference is well represented in all but the thinnest sand as well.

Case 2: Point electrode to casing configuration.

As an intermediate step toward a pure casing-to-casing configuration, we next simulated a hybrid configuration utilizing both point electrodes and vertical casings as long electrodes (Figure

2). These simulations were computed in 3D. We assume two electrode arrays, 23.3 m apart, with a vertical casing outboard on each side, an additional 23.3 m out. Two surface electrodes were included, each located an additional 94 m outboard of the two casings. The finite difference mesh width is 1554 m in the direction co-planar with the casings and electrode arrays, 1508 m in the direction perpendicular to the image plane, and 786 m deep. The imaged plane lies in the center. The point electrode arrays are shown schematically in the figure; they are located in the same 98 m interval as in the first case. The model is only permitted to change between 348 and 446 m; this assumes changes only occur in the pay zone.

In this simulation, we permit the resistivities of the initially 40 ohm-m sand units to decrease to 10 ohm-m, simulating the progress of steam through the sands over time. The lower sand unit reaches only partway across the image plane. Steam fills from right to left. The decrease in resistivity due to the passage of steam is apparent in the time progression of the inverted difference images (with respect to baseline) (Figure 2). The location and amplitude of the steam front is well reproduced between and near the point electrodes. Resolution is lost (the image appears smeared) near the vertical casings.

Case 3: Casing to casing configuration.

In the casing to casing configuration models, we modeled the electrode array as a simple 9-spot pattern of vertical casings acting as electrodes (Figures 3 and 4). The casings define a square pattern which is 140 m on a side. Twelve surface electrodes were included, located halfway between each of the nine casings, in the x and y directions. The complete model width is 2270.28 m in both the x and y directions, and is 956.24 m deep. The imaged volume lies in the center, in the depth interval from 348 to 446 m.

We considered two cases. In the first, the entire 445 m long casings were utilized as a “long” electrode (Figure 3). In the second, only the lower 70 m of each casing was energized, simulating a “short” electrode over the lower portion of the casing (Figure 4). This latter configuration reflects engineering considerations for limiting current flow over the upper portion of the casing above the region of interest. In both cases, the model is only permitted to change between 348 and 446 m. As before, the model consists of 40 ohm-m sands, filling over time with 10 ohm-m steam, surrounded by a 4 ohm-m shale. Steam fills from right to left, and only fills part of the volume (plane in and out of the page). All changes are constrained to the lower portion of the model.

In both the “long” and “short” casing to casing simulations, no vertical resolution is available. However, there is useful horizontal resolution. The movement of steam across the field is readily apparent, particularly in the difference images. The lateral extent in both the along- and across- steam front directions is well reproduced. The long model predicts a smaller difference amplitude than expected. The short model results in a greater predicted amplitude of the difference, closer to the expected value.

Summary

We have evaluated the use of metal casings as long electrodes with which to perform electrical resistance tomography. The results of these simulations suggest that it may be possible to monitor steam flood using this approach. Conventional crosswell ERT provides good lateral

and vertical images of resistivity changes resulting from steam progress. In the hybrid case, using both vertical casings and point electrode arrays, overall resolution was degraded with respect to the crosswell electrode string case, yet better than that using casings alone, as expected. Using vertical casings alone, there is distinct signature indicative of the changing resistivity across the field, which is well above the noise level in the simulations. Given these indications, field surveys in an oil field undergoing steam flood are underway.

Acknowledgements

This work was funded by the U.S. Department of Energy's Office of Fossil Energy, Natural Gas and Oil Technology Partnership program. We appreciate the efforts of Rhonda Lindsey, the National Petroleum Technology Office Program Manager for this project. We gratefully acknowledge the support of our industrial partners, Aera Energy LLC, Chevron Production, Inc. and SteamTech Environmental Services, Inc., in this effort. Work performed under the auspices of the U.S. Department of Energy by the Lawrence Livermore National Laboratory under Contract W-7405-ENG-48.

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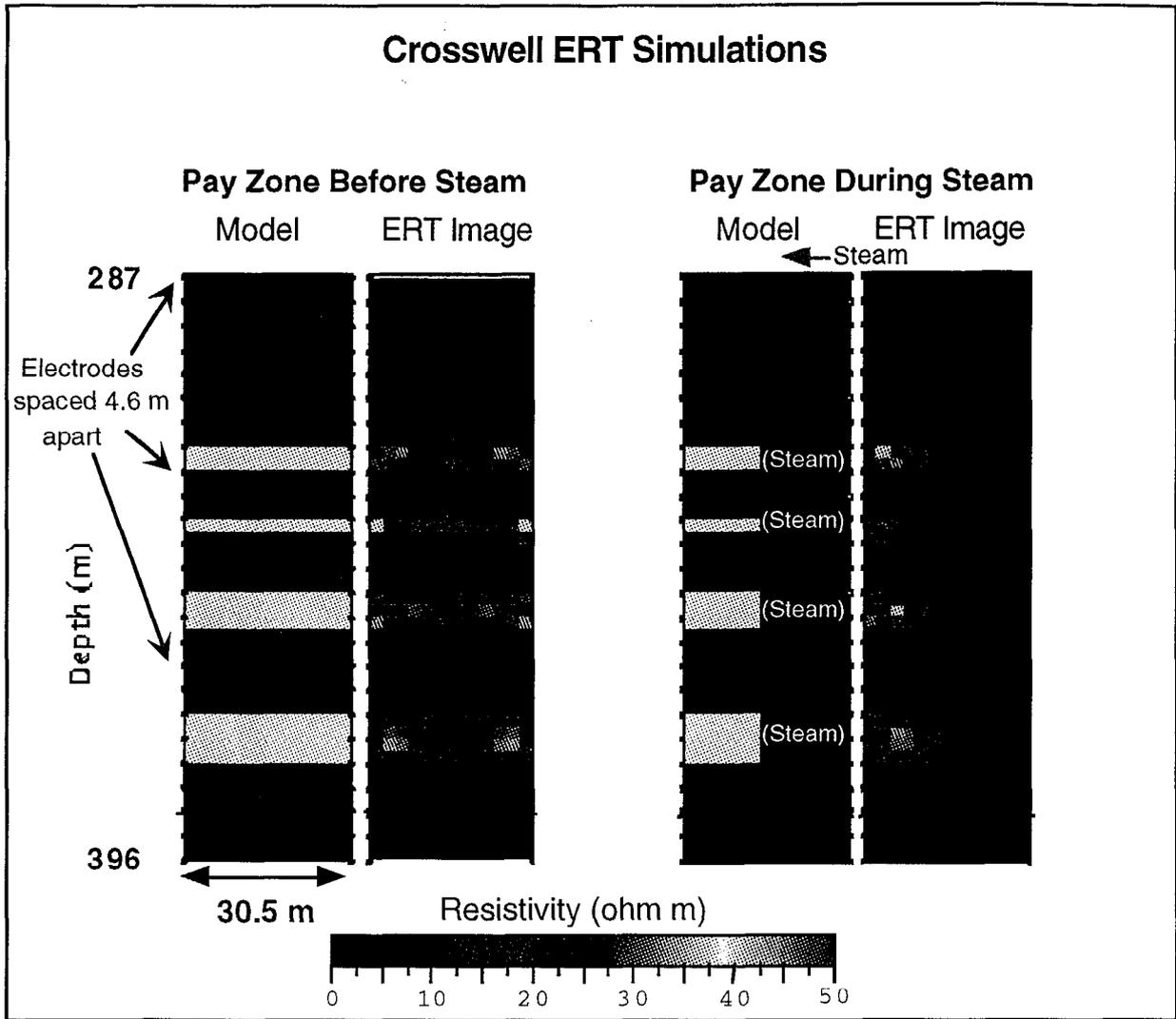
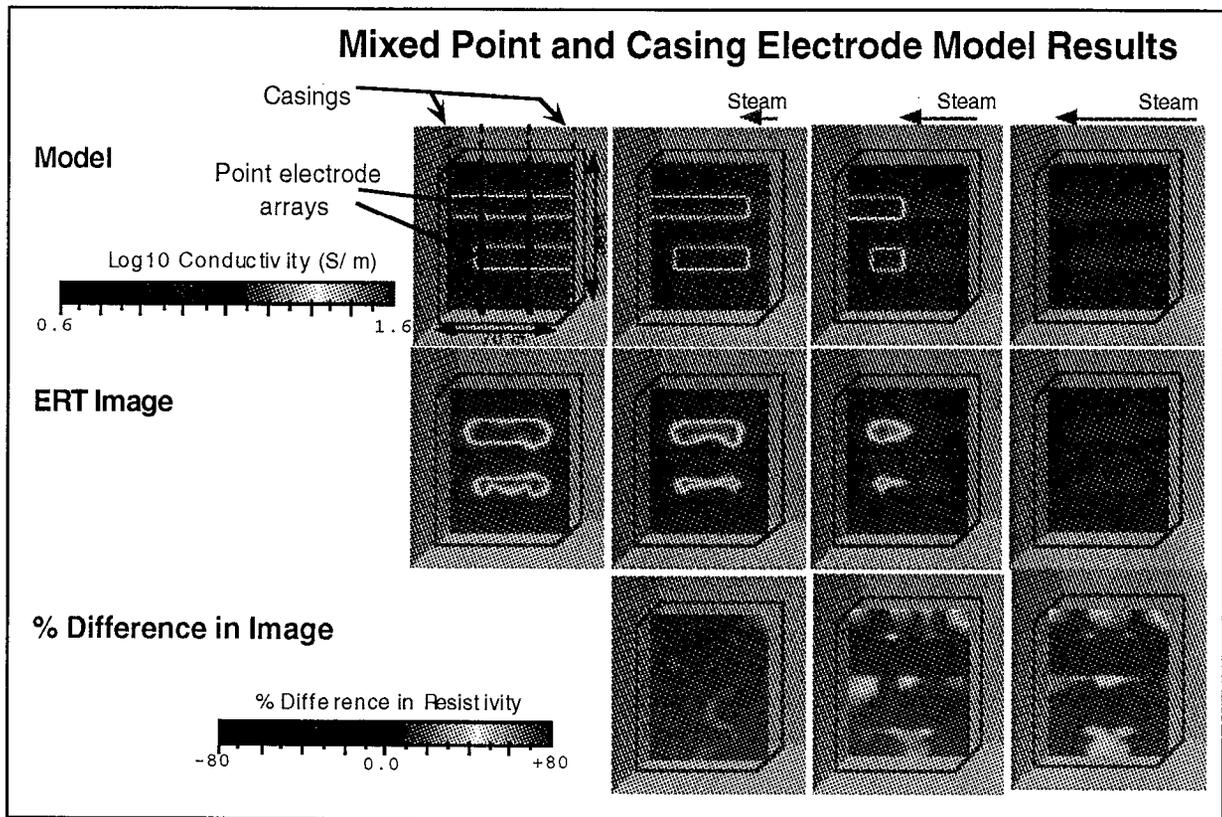


Figure 1. Crosswell ERT simulations, showing the effect of various thickness sand units filling time, decreasing their resistivity to that of the surrounding shale. On the left are shown the model and the inverted ERT image. On the right are shown the model and inversion assuming that the steam has passed halfway through the image plane, in all the sand units.

Figure 2. Results of simulating mixed point and casing electrodes. Top: 3D model, with 40 ohm m sands, filling over time with 10 ohm m steam, surrounded by a 4 ohm m shale. Steam fills from right to left; the lower sand unit reaches only partway across the image plane. Center: Simulated inversions. Bottom: Difference images (with respect to baseline) over time.



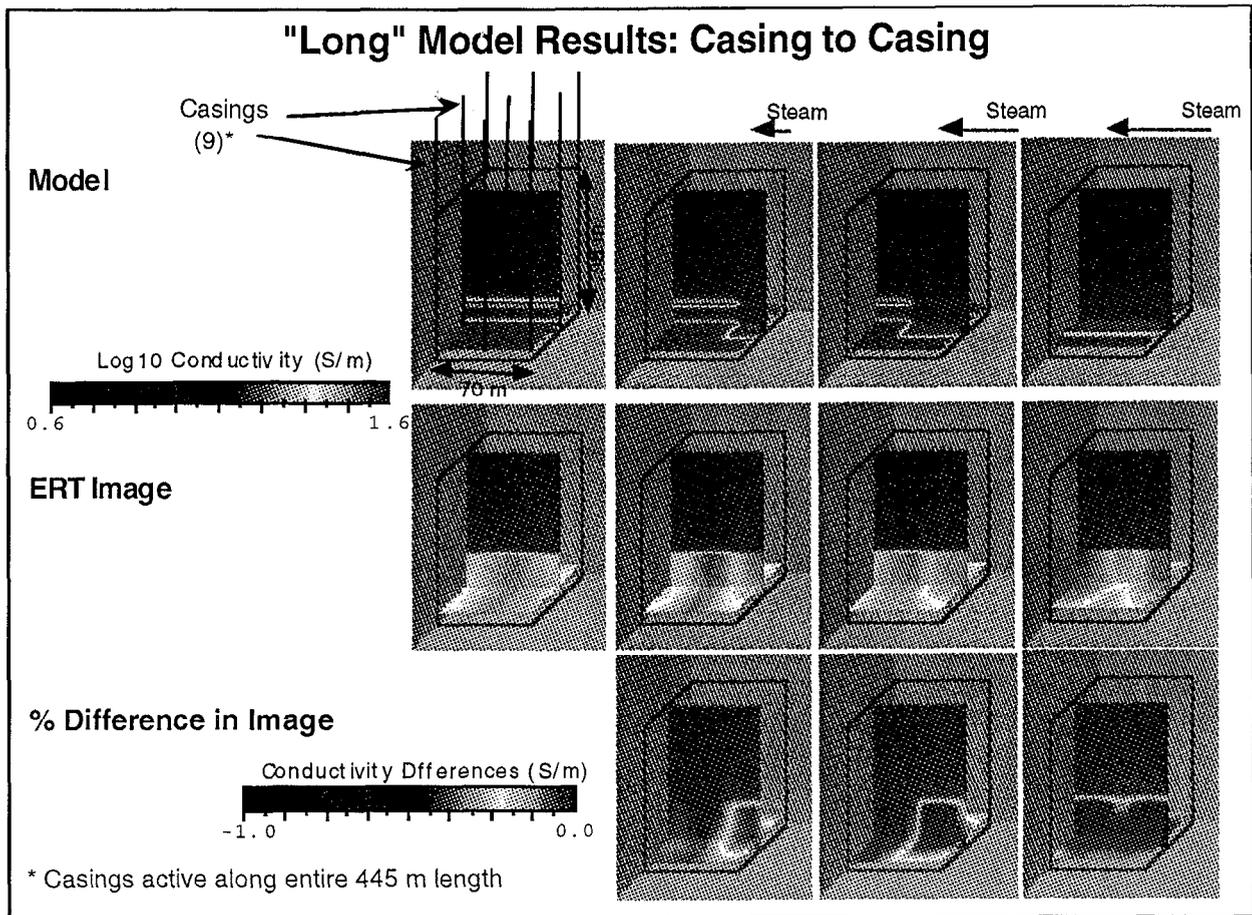


Figure 3. Results of "long" casing-to-casing simulations, assuming the entire casing length has electrical contact with the formation. Steam fills from right to left, and only fills part of the volume (plane in and out of the page). Center: Simulated inversions. Bottom: Difference images (with respect to baseline) over time. All changes are constrained to the lower portion of the model.

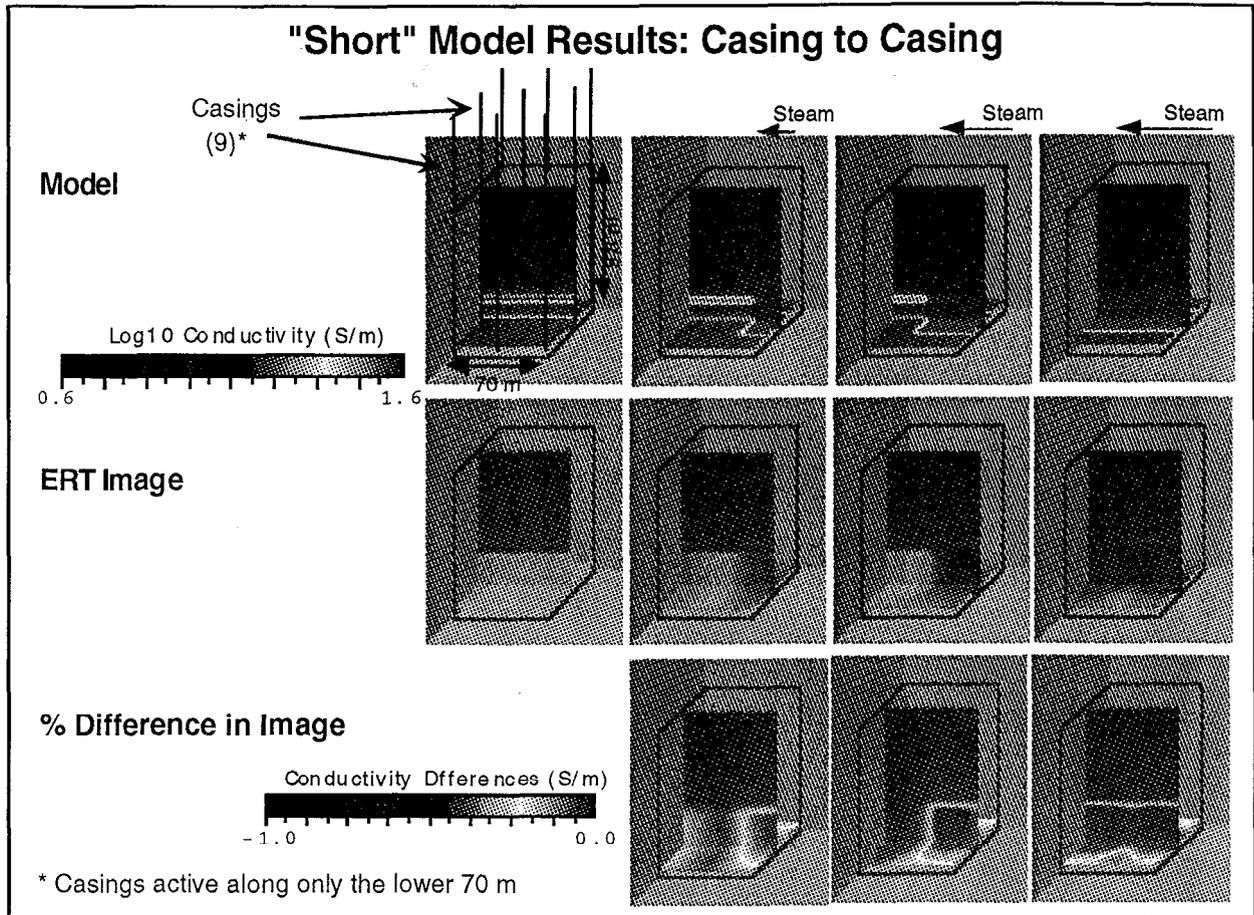


Figure 4. Results of "short" casing-to-casing simulations, assuming only the lower 70m of casings have electrical contact with the formation. Same presentation as in Figure 3.