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Initial Dislocation Structure and Dynamic Dislocation Multiplication in Mo Single Crystals

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INITIAL DISLOCATION STRUCTURE AND DYNAMIC DISLOCATION MULTIPLICATION IN Mo SINGLE CRYSTALS

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Summary

Initial dislocation structure in annealed high-purity Mo single crystals and deformation substructure in a crystal subjected to 1% compression have been examined and studied in order to investigate dislocation multiplication mechanisms in the early stages of plastic deformation. The initial dislocation density is in a range of $10^6 \sim 10^7 \text{ cm}^{-2}$, and the dislocation structure is found to contain many grown-in superjogs along dislocation lines. The dislocation density increases to a range of $10^8 \sim 10^9 \text{ cm}^{-2}$, and the average jog height is also found to increase after compressing for a total strain of 1%. It is proposed that the preexisting jogged screw dislocations can act as (multiple) dislocation multiplication sources when deformed under quasi-static conditions. Both the jog height and length of link segment (between jogs) can increase by stress-induced jog coalescence, which takes place via the lateral migration (drift) of superjogs driven by unbalanced line-tension partials acting on link segments of unequal lengths. Applied shear stress begins to push each link segment to precede dislocation multiplication when link length and jog height are greater than critical lengths. This dynamic dislocation multiplication source is subsequently verified by direct simulations of dislocation dynamics under stress to be crucial in the early stages of plastic deformation in Mo single crystals.

Introduction

The main purpose of this study is to examine, analyze the initial dislocation structure and deformation substructure of Mo single crystals in order to provide detailed physical mechanisms to facilitate multi-scale modeling and dislocation dynamics simulation [1]. For the success of simulation, it is of paramount importance to have a systematic and rigorous study on dynamic properties of dislocations including dislocation multiplication, motion, and dislocation interaction. Since the initial dislocation structures (dislocation density, dislocation configuration, free dislocation link length, kink and jog density...) can all affect dislocation dynamics during subsequent plastic deformation, the dislocation substructures in as-annealed and quasi-statically compressed Mo crystals were studied and compared. Emphasis has been placed upon the role of initial dislocation structures in dislocation multiplication and motion during early stages of plastic deformation.

Experimental

The Mo single crystals used for dislocation dynamics experiment must have low dislocation density in order to analyze the structure with TEM and to subsequently establish initial conditions for simulation. Mo single crystals were obtained from Accumet Materials Company, Ossining, NY. The interstitial impurities (ppm in weight) in Mo are O: 25; N: <10; H: <5; C: <10, respectively. Prior to compression test, the test sample was heat treated at 1500°C for 1 h, 1200°C for 1 h, and 1000°C for 1 h at a vacuum of 8×10^{-11} Torr. Testing of single crystals involves compressing the test sample between two platen surfaces under precise conditions. To measure shear strain during compression, a 3-element rosette gage was bonded in the gage section on each side of the sample. The gages were applied with room temperature curing epoxy adhesive. A compression test was performed on a Mo test sample with a $[118]$ compression axis. This orientation was chosen to study single-slip deformation involving the $(\bar{1}\bar{1}2)[111]$ slip system. The sample was compressed at a nominal strain rate of 10^{-3} S^{-1} . The sample was compressed to a value of approximately 1% axial strain. TEM foils were sliced from the gage section of the tested piece with the foil sliced parallel to the $(\bar{1}\bar{1}2)$ plane. TEM specimens were finally prepared by a standard twin-jet electropolishing technique in a solution of 75 vol.% ethanol and 25 vol.% sulfuric acid at $\sim 25 \text{ V}$ and -10°C .

Results and Discussion

Initial dislocation structure in annealed crystals

Figure 1 shows the initial dislocation structures observed from the $[011]$ -, $[0\bar{1}1]$ - and $[100]$ -sliced foils, which are illustrated here on the three surfaces of a box. The dislocation density (ρ) is estimated to be on the order of $10^6 \sim 10^7 \text{ cm}^{-2}$. Occasionally, cross-grid screw dislocations with Burgers vectors of $\pm \frac{1}{2} [111]$ and $\pm \frac{1}{2} [1\bar{1}\bar{1}]$ were observed in the $[0\bar{1}1]$ -sliced foil, which were determined using the $\mathbf{g} \cdot \mathbf{b} = 0$ invisible criterion as shown in Fig. 2. As can be seen clearly that the dislocations of $\mathbf{b} = \pm \frac{1}{2} [1\bar{1}\bar{1}]$ become invisible when $\mathbf{g} = 2\bar{1}\bar{1}$ is applied for imaging, and those of $\mathbf{b} = \pm \frac{1}{2} [111]$ become invisible when $\mathbf{g} = 2\bar{1}\bar{1}$ is applied for imaging. These dislocation pairs have a near-screw character since their line vectors are nearly parallel to their Burgers vectors. Notice that the appearance of residual contrasts under $\mathbf{g} \cdot \mathbf{b} = 0$ conditions suggests that these dislocation lines are not pure screw in character.

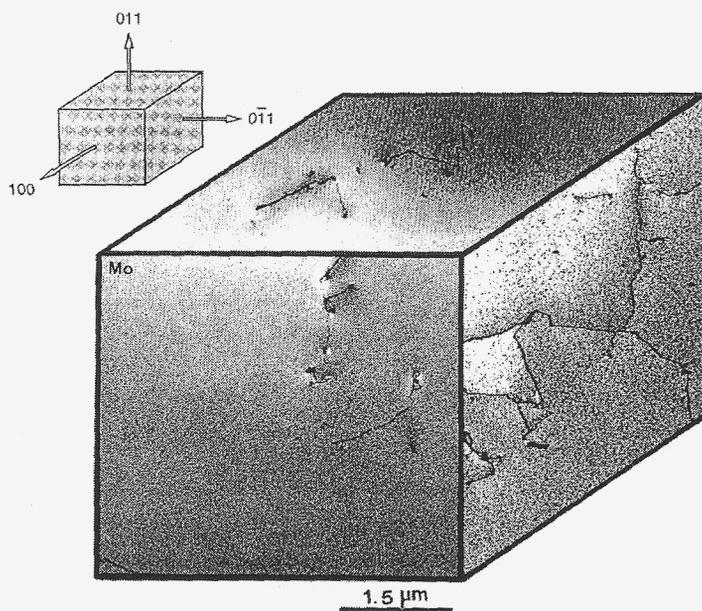


Fig. 1. Initial dislocation structure in as-annealed Mo single crystals.

According to Frank-Read dislocation multiplication mechanism [2], dislocation can multiply by repeatedly bowing out a free segment of dislocation line lying in a slip plane, and the shear stress (τ) required bowing out a line segment (l) is given as: $\tau \approx \mu b/l$. Thus, there may exist a critical length ($l^* \approx \mu b/\tau_a$) of free segment for a given applied shear stress (τ_a). Any length of free segment l which is smaller than l^* will be permanently immobile, while length of segment greater than l^* are potentially mobile. Accordingly, an investigation of the relative density (ρ_m/ρ) of mobile dislocation in slip plane is important for studying the yield strength of crystal. An investigation made on this aspect of dislocation configuration is shown in Fig. 3. Here, an "in-plane" $\frac{1}{2}[111]$ dislocation segment ($\sim 5 \mu\text{m}$ in length) in the $\{0\bar{1}1\}$ plane is shown. Notice the bend-over at two ends of the segment, which indicates that a dislocation line is not entirely lying in one crystallographic plane. However, there is an uncertainty whether the observed segment is truly a free dislocation segment without any other pinning points such as short jog segments formed on the dislocation line. In other words, there is a difficulty to define free segment length by viewing dislocation from this orientation since it is infeasible to locate the pinning points formed by jog segments along the dislocation line.

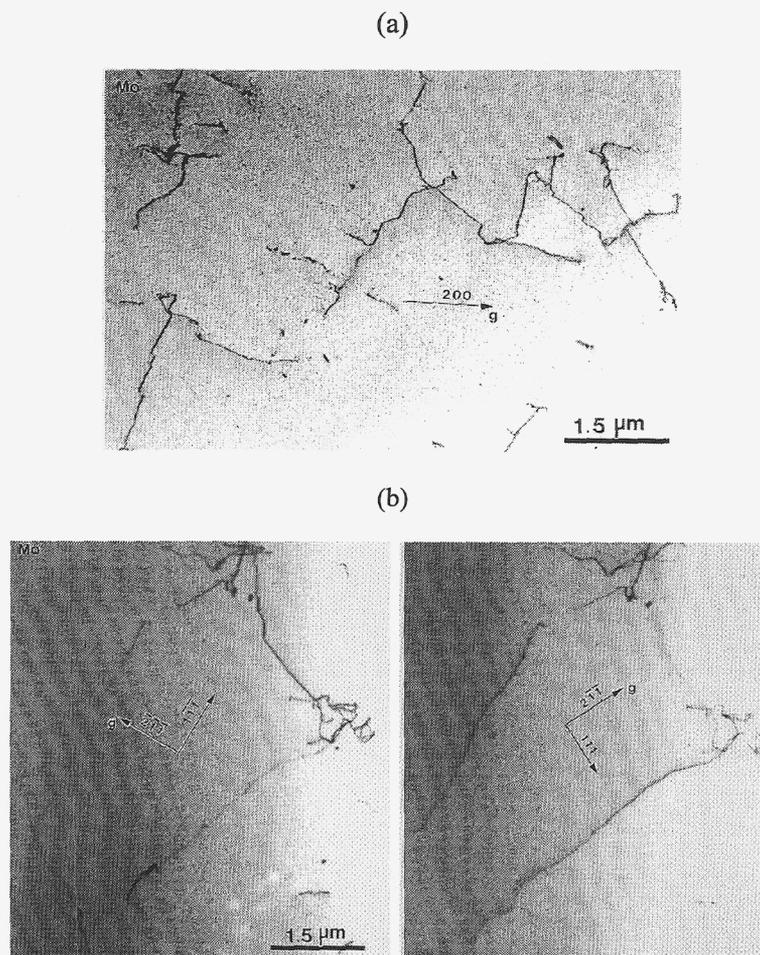


Fig. 2. Bright-field TEM images showing (a) the formation of cross-grid dislocations, and (b) a $\mathbf{g}\cdot\mathbf{b}$ analysis for the character of cross-grid dislocations; (left) \mathbf{Z} (zone axis) $\approx [0\bar{1}1]$, $\mathbf{g} = 2\bar{1}1$, dislocations of $\mathbf{b} = \pm \frac{1}{2} [111]$ become invisible, and (right) $\mathbf{Z} \approx [0\bar{1}1]$, $\mathbf{g} = 2\bar{1}1$, dislocations of $\mathbf{b} = \pm \frac{1}{2} [1\bar{1}\bar{1}]$ become invisible.

In fact, the dislocation segment length viewed from the $\{\bar{1}01\}$ -sliced foils may be a measure of the line waviness along the foil normal. This can be visualized readily from a cross-sectional view of $\frac{1}{2}[\bar{1}\bar{1}1]$ screw dislocation shown in Fig. 4(a), in which the screw dislocation in the (011) plane was observed from the foil sliced parallel to the (0 $\bar{1}1$) plane. Here, the existence of many long superjogs (50 ~ 100 nm in height) along the $\frac{1}{2}[\bar{1}\bar{1}1]$ screw dislocation line can be seen. In addition, the dislocation line is found to skew away from the $[\bar{1}\bar{1}1]$ direction revealing that the dislocation line is also associated with many short superjogs [jog height (d) < 1 nm] or elementary jogs [jog height = interplanar spacing of ($\bar{1}21$) plane = 0.135 nm]. Noted that the height of short superjogs or elementary jogs is too short to be resolvable using conventional TEM imaging techniques. This examination suggests that the short dislocation segments appeared in the $\{\bar{1}01\}$ -sliced foils is attributed to the formation of jogs along a screw dislocation line which causes it to lie across many $\{\bar{1}01\}$ planes instead of one. Consequently, screw dislocation lines are chopped into short segments in a $\{\bar{1}01\}$ -sliced TEM foils (~ 0.4 μm thick). Similarly, jogged $\frac{1}{2}[111]$ and $\frac{1}{2}[1\bar{1}\bar{1}]$ screw dislocations were also observed. A jogged $\frac{1}{2}[1\bar{1}\bar{1}]$ screw dislocation viewed from the $[0\bar{1}1]$ direction is shown in Fig. 4(b). Here, many large superjogs (50 ~ 100 nm in height) can be readily seen along the dislocation line. Also notice that the lengths of each free segment linked between two superjogs are unequal.

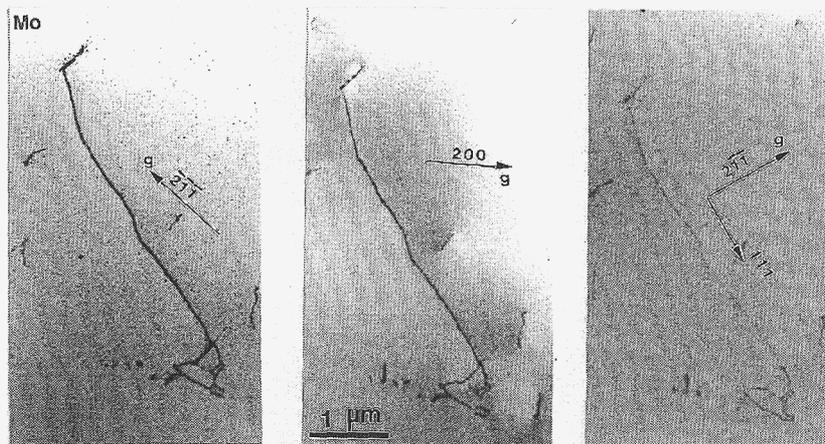


Fig. 3. A $g\cdot b$ analysis for a $\pm \frac{1}{2} [111]$ screw dislocation formed in $(0\bar{1}1)$ -sliced Mo.

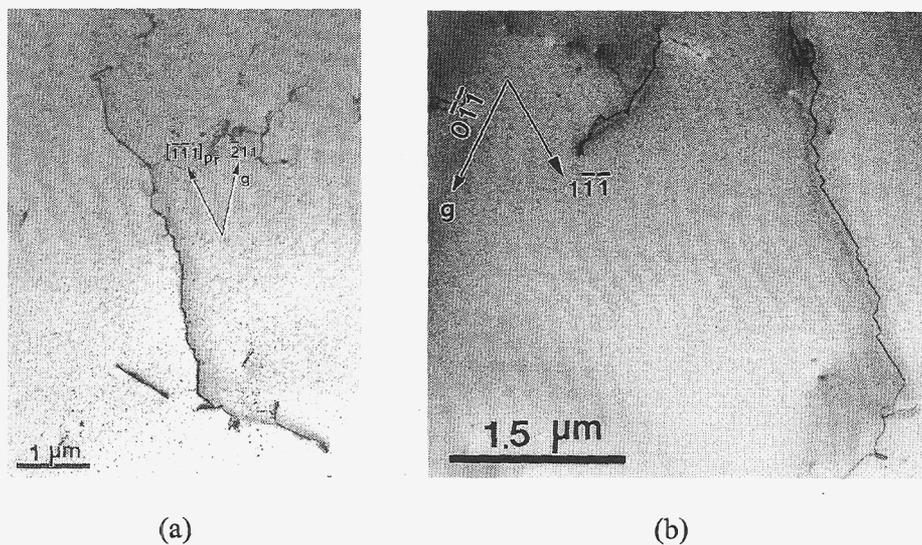


Fig. 4. TEM images showing (a) a jogged $\frac{1}{2}[\bar{1}\bar{1}1]$ screw dislocation and (b) a jogged $\frac{1}{2}[1\bar{1}\bar{1}]$ screw dislocation viewed from the $[011]$ direction in as-annealed Mo.

Deformation substructure

Typical deformation substructures of a crystal compressed for 1 % are shown in Fig. 5. The dislocation density increases about two orders of magnitude to a range of $10^8 \sim 10^9 \text{ cm}^{-2}$. Although the $\frac{1}{2}[111]$ screw dislocations are prevalent, other secondary dislocations are also operative. Notice that many superjogs (marked by arrows) are seen along screw dislocation lines, and the average jog height, and free segment between superjogs are found to increase significantly in comparison with that observed in as-annealed samples (Fig. 4). In addition, the screw dislocation lines become much straighter and longer comparing to those in as-annealed crystals. The increase of cross-grid screw dislocations, as shown in Fig. 5(b), indicates that multiple slip systems have been activated in the early stage of plastic deformation. It is worth noting that few junction dislocations are formed at the cross points of the cross-grid dislocations during the stage.

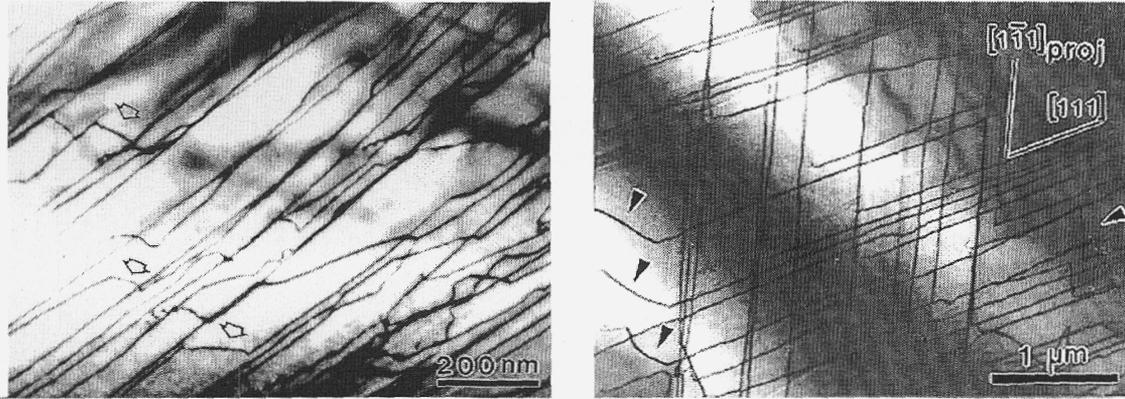


Fig. 5. Typical dislocation structures observed in a crystal compressed for 1 %.

Dislocation multiplication mechanisms

Based upon TEM results shown in Figs. 4 and 5, dislocation multiplication during the early stage of plastic deformation in Mo single crystals can be rationalized by mechanisms proposed and illustrated in Fig. 6. Here, screw dislocation segments (pinned by superjogs) bow out between the superjogs under an applied shear stress (τ) to a certain curvature, yet they are immobile since the initial length (l_0) of each free segment is smaller than a critical length ($l^* \approx \mu b/\tau$) as defined earlier. Beside the force exerted on dislocation segments by the applied shear stress, each superjog is subjected to a net force (F_x) parallel to the Burgers vector due to the bowing of unevenly spaced link segments between jogs under small strains, which is schematically illustrated in Fig. 6 (d). The magnitude of net force can be expressed as:

$$F_x = \Gamma(\cos\phi_2 - \cos\phi_1),$$

where $\phi = \sigma b l / 2\Gamma$, and Γ is the line tension. Applying Taylor expansion to $\cos\phi$, thus

$$F_x \approx \frac{b^2 \sigma^2}{8\Gamma} (l_1^2 - l_2^2).$$

The force causes large loop to grow at the expense of neighboring short loop by drifting the jog at P. The jog drifting velocity (v_j) can be related to the mobility (D_j/kT) by the Einstein mobility relation [3, 4]

$$v_j = \frac{D_j}{kT} F_x$$

where D_j is the jog diffusivity. That is, each jog in Fig. 7(b) moves in such a direction so that the shorter segments (**CD** and **EF**) become still shorter and the longer segments (**AB** and **GH**) are expanded [5]. The jogs of like-sign tend to coalesce in order to reduced line energy and resulting in the increase of jog height [6]. Consequently, the stress-induced jog pileup and coalescence renders an increase of both segment length and jog height.

Applied shear stress eventually begins to push each line segment between jogs to precede dislocation multiplication when the length of line segments (**IJ** and **KL**) and height of superjog (**JK**) are greater than critical values, i.e.

$$l^* \approx \mu b / \tau,$$

and

$$d_c \approx \mu b / 8\pi(1-\nu)\tau.$$

Here, a mutual attraction force between adjacent bowing edge segments of opposite signs can define d_c . That is, the originally immobile screw dislocations become multiple sources for dislocation multiplication as a result of the jog coalescence process. This "dynamic" dislocation multiplication source is suggested to be crucial for the dislocation multiplication in the early stage of plastic deformation in Mo.

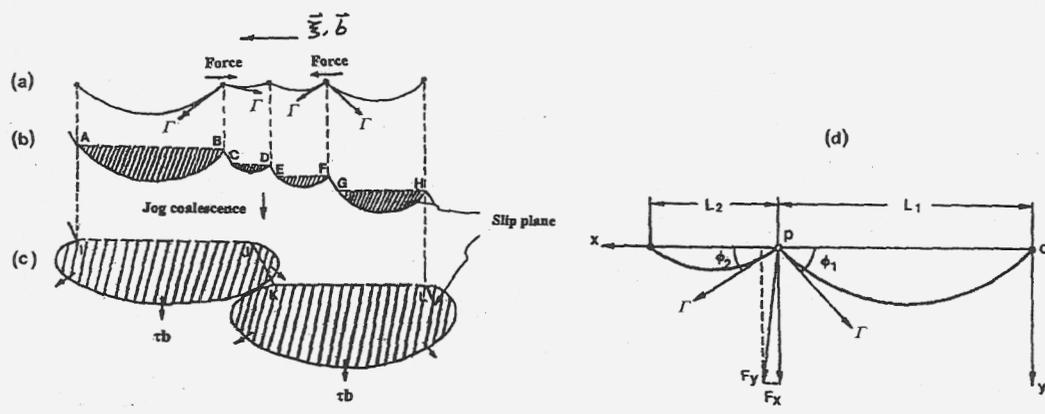


Fig. 6. Schematic illustrations of dislocation multiplication from a jogged screw dislocation. (a) A top view showing dislocation segments pinned by superjogs bowing under stress to a curvature, net forces are generated on jogs due to unbalanced line-tension partials acting on the free segments of unequal lengths. (b) A tilt view of (a) shows the initial heights of like-sign superjogs. (c) Both segment length and jog height increase due to stress-induced jog coalescence. As a result, two multiplication sources are generated at segments \overline{IJ} and \overline{KL} . (d) The resolved forces F_x and F_y acting on the jog (pinning point) caused by link segments of unequal lengths, L_1 and L_2 bowing under low strains.

Conclusion

Screw dislocations in association with grown-in superjog segments were observed within annealed Mo single crystals. It is proposed that the jogged screw dislocations can act as a dynamic multiplication source for dislocation multiplication when deformed at quasi-static conditions as a result of stress-induced migration and coalescence of superjogs. The jog coalescence can take place via the lateral migration (drift) of jog segments driven by unbalanced line tension partials acting on line segments (between jogs) of unequal lengths. The coalescence of jog segments results in the increase of both segment length and jog height. The jog coalescence continues until the segment length and jog height are greater than critical values so that applied stress begins to push each line segment to precede multiple dislocation multiplication.

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