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# THE ENERGY DIAMETER EFFECT

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**Abstract.** Various relations for the detonation energy and velocity as they relate to the inverse radius of the cylinder are explored. The detonation rate-inverse slope relation seen in reactive flow models can be used to derive the familiar Eyring equation. Generalized inverse radii can be shown to fit large quantities of cylinder and sphere results. A rough relation between detonation energy and detonation velocity is found from collected JWL values. Cylinder test data for ammonium nitrate mixes down to 6.35 mm radii are presented, and a size energy effect is shown to exist in the Cylinder test data. The relation that detonation energy is roughly proportional to the square of the detonation velocity is shown by data and calculation.

**Keywords:** size effect, diameter effect, detonation velocity, detonation energy, cylinder test

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The size (diameter) effect is the well known decrease of detonation velocity with decreasing radius. Plotting the detonation velocity as a function of inverse radius [1], the extrapolation to zero produces the detonation velocity at infinite radius, which should be what is calculated by CHEETAH [2] or any thermo-chemical code. We have suggested that, as the radius decreases, the fraction of the explosive that remains unburned increases [3]. In terms of the burn fraction,  $F_e$ , which is the fraction of explosive burned, we estimated that

$$F_e = \frac{E_0}{E_0^D} \approx \left( \frac{U_s}{D} \right)^2, \quad (1)$$

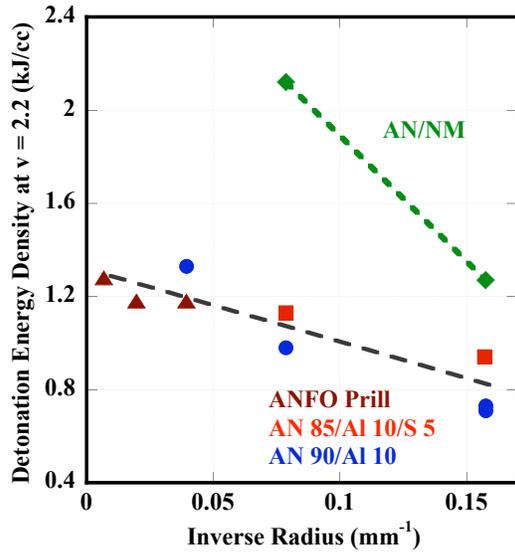
where  $F_e$  is the burn fraction at the back of the reaction zone,  $E_0$  and  $U_s$  are the detonation energy and velocity at some radius  $R_0$ , and  $E_0^D$  and  $D$  are the same at infinite radius. While this relation was derived assuming a single overall chemical reaction, which is not true, it is helpful in estimating energetic effects.

Is it possible to see this effect in measured data from the Cylinder test, where the square of the copper velocity is proportional to the detonation energy at three standard relative volumes [4, 5]? This test has traditionally been used on near-ideal explosives, where changes of cylinder size have little effect. Shots using ANFO have tended to be large in order to avoid non-ideal effects. Here, we deliberately shrink the copper cylinder down to as little as 6.35 mm inner radius in order to look for the energy effect. Also, we use explosives near half-density, which are weak, but tend to continue detonating down to small sizes.

Table 1 lists the data taken recently on ammonium nitrate mixes in small size cylinders. This data is plotted in Figure 1 as a function of inverse radius and a size effect is seen. The energy is at the relative volume of 2.2, which corresponds to the scaled outer wall displacement of 6 mm. This relative volume, which is the first of the cylinder standards, is often taken as a measure of the metal-pushing power of the explosive.

**Table 1.** Copper cylinder shots for various ammonium nitrate mixes.

Explosive	density		Det Velocity ( $\mu\text{s}$ )	Expl. Radius (mm)	Cu thick (mm)	Measured Scaled Wall Velocity (mm/ $\mu\text{s}$ )			Det Energy Density, $E_d$ (kJ/cm <sup>3</sup> )		
	(g/cm <sup>3</sup> )	remarks				6	12.5	19	2.2	4.4	7.2
	AN 85/Al 10/S 5	0.988				5 $\mu\text{m}$ Al	3.375	12.7	2.52	0.670	0.785
AN 85/Al 10/S 5	0.993	5 $\mu\text{m}$ Al	2.952	0.000	1.36	0.588	0.692	0.743	0.94	1.25	1.41
AN 90/Al 10	1.044	5 $\mu\text{m}$ Al	3.673	25.41	5.21	0.712	0.821	0.888	1.33	1.70	1.95
AN 90/Al 10	1.002	95 $\mu\text{m}$ Al	3.486	25.43	5.19	0.674	0.782	0.835	1.18	1.53	1.71
AN 90/Al 10	1.023	20 $\mu\text{m}$ Al	3.068	12.72	2.58	0.614	0.724	0.782	0.98	1.30	1.49
AN 90/Al 10	1.023	20 $\mu\text{m}$ Al	2.644	6.35	1.36	0.516	0.595	0.642	0.73	0.93	1.06
AN 90/Al 10	1.023	20 $\mu\text{m}$ Al	2.644	6.35	1.36	0.509	0.601	0.658	0.71	0.95	1.12
AN 79/NM 21	1.20	Kinepak	5.134	12.705	2.606	0.890	0.967	1.008	2.12	2.40	2.56
AN 79/NM 21	1.05	Kinepak	3.923	6.350	1.360	0.680	0.782	0.827	1.27	1.61	1.77



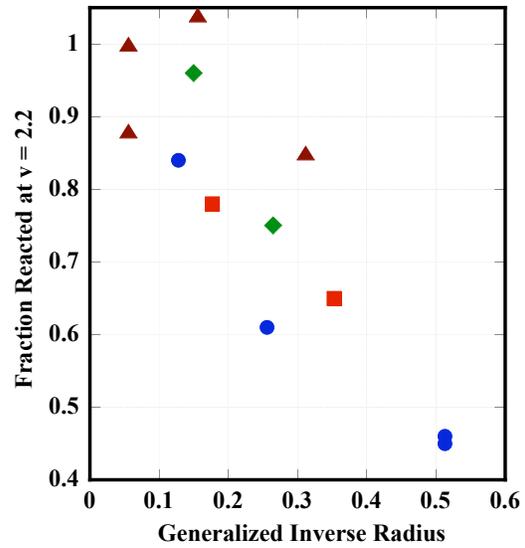
**Figure 1.** Size effect for explosives at a relative volume of 2.2. The explosives are: AN/NM (diamonds), ANFO prill (triangles), AN/Al/S (squares) and AN/Al (circles).

We can go to the next step. We define the burn fraction,  $F$ , as being the measured cylinder energy divided by the calculated CHEETAH energy, all at a given relative volume. Also, we can define a generalized inverse radius given by

$$\left(\frac{1}{R_0}\right)_g = \frac{D}{\langle v \rangle R_0} \quad (2)$$

where  $\langle v \rangle$  is the average detonation rate in  $\mu\text{s}^{-1}$  [3]. This plot is shown in Figure 2 and the

higher rate AN/NM is brought into line with the other points.



**Figure 2.** Generalized inverse radius plot derived from Figure 1. The same notation is used.

Next, we go to our JWL library for all explosives and plot the total detonation energy,  $E_0$ , and the detonation energy at  $v = 2.2$ ,  $E_d(2)$  as a function of detonation velocity.  $E_0$  is a somewhat mythical concept because it requires expansion of the gas products to infinite volume, so the extrapolated value from CHEETAH is usually used. The result of all these values is given by

$$\begin{aligned} E_d(2) &\propto U_s^{2.2} \\ E_o &\propto U_s^{1.6} \end{aligned} \quad (3)$$

The last step toward Eq. 1 requires knowing  $D$ , the infinite radius detonation velocity. This can be calculated using CHEETAH, but thermochemical codes have most trouble with detonation velocities. It can be had by extrapolating the size effect data, but most of the data is on small cylinders, so that few points near zero are available. Also, extremely non-ideal explosives often have concave-up shapes, so that  $D$  is larger than we think. The results are shown in Figure 4 and the dashed line fitted to Eq. 1 is just slightly below the data.

We finally calculated the burn fraction using simple JWL++ with a single detonation rate [6] and these results are shown in Figure 5. The simple reactive flow model also incorporates a close version of Eq. 1.

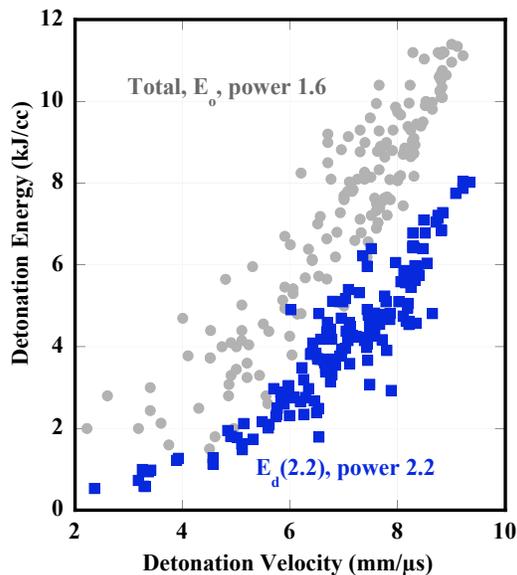


Figure 3. Near-squared dependence of energies taken from JWL's.

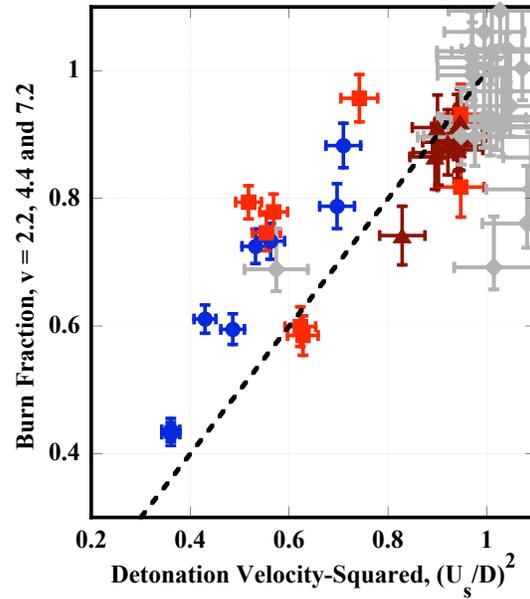


Figure 4. Cylinder test burn fractions versus dimensionless detonation velocity-squared. The points are: AN mixes, this paper (circles), older AN mixes (squares), LX-17 (triangles) and other (diamonds). The dashed line is Eq. 1.

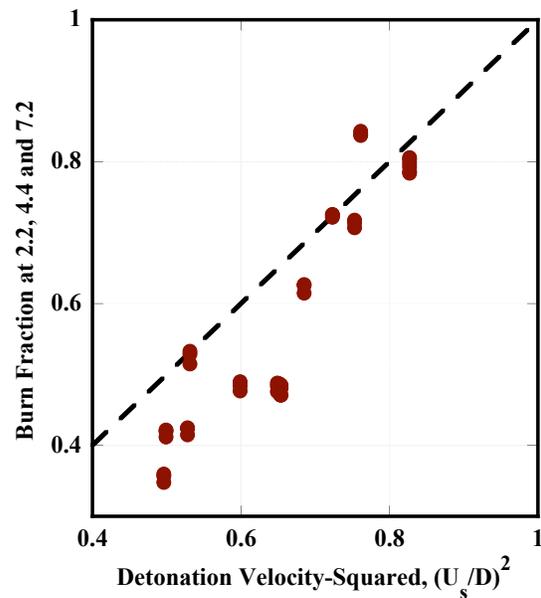


Figure 5. Calculated AN 90/Al 10 burn fractions versus dimensionless detonation velocity-squared with the dashed line being Eq. 1.

In conclusion, the data does support the idea of an energy size effect.

## ACKNOWLEDGMENTS

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